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Acoustic optimisation of a fan test rig

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FFT ACOUSTIC SIMULATION
CONFERENCE **2014**
Actran Users' Meeting



AneCom aerotest facility

Specialist test rig for measuring the aerodynamic performance and noise of aero-engine fans

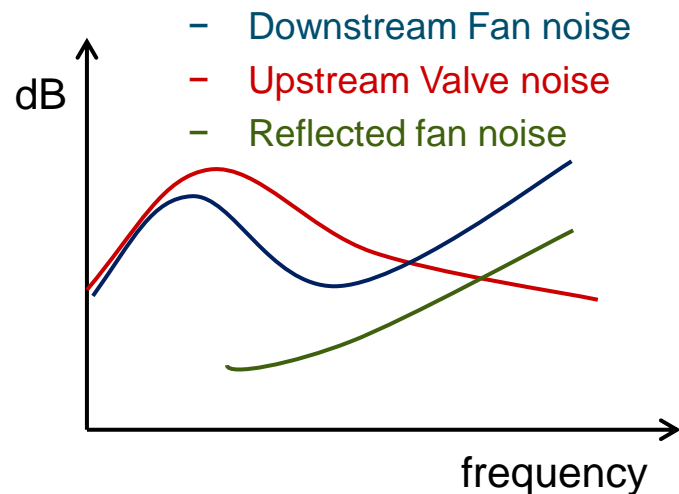


- **Undergoing re-design to increase flow capacity without bypass duct noise measurement contamination**
 - Noise generated by the flow control throttle
 - Acoustic reflections from the throttle
- **Despite a strong constraint in space available**
- **Actran TM used in order to**
 - Attenuate throttle noise by 20dB
 - Reduce power reflection coefficient to below -8dB
 - Wide range of frequency of interest (250 – 4000 Hz)

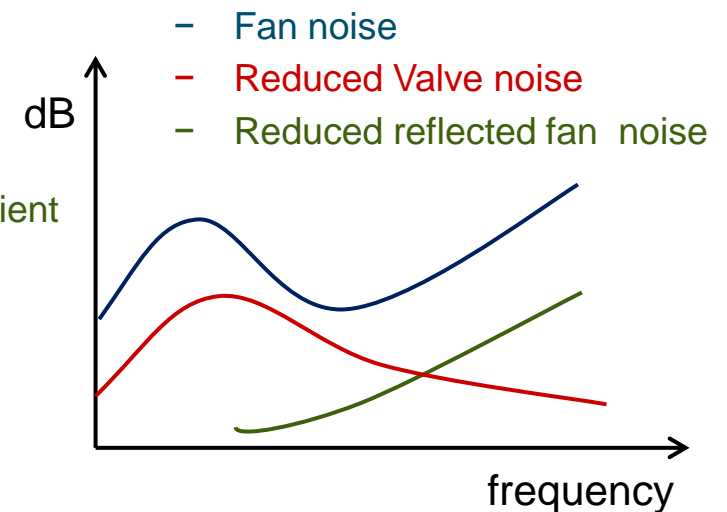
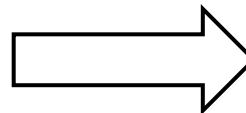
Fan noise test challenge

Accurate measuring of fan noise propagating downstream is helped by a reduction of noise propagating upstream:

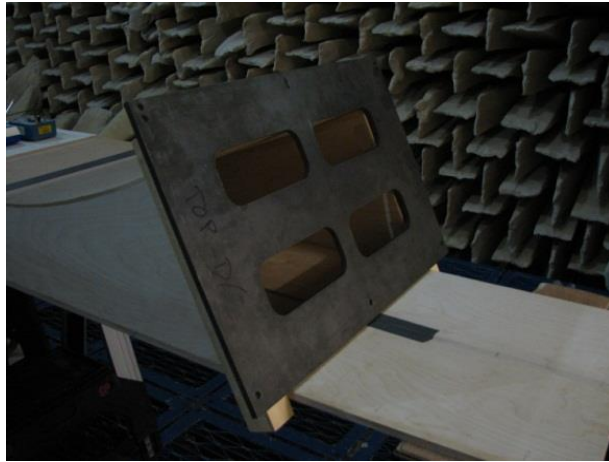
1. Valve noise
2. Reflected fan noise



- Attenuate Valve noise
- Reduce reflection coefficient

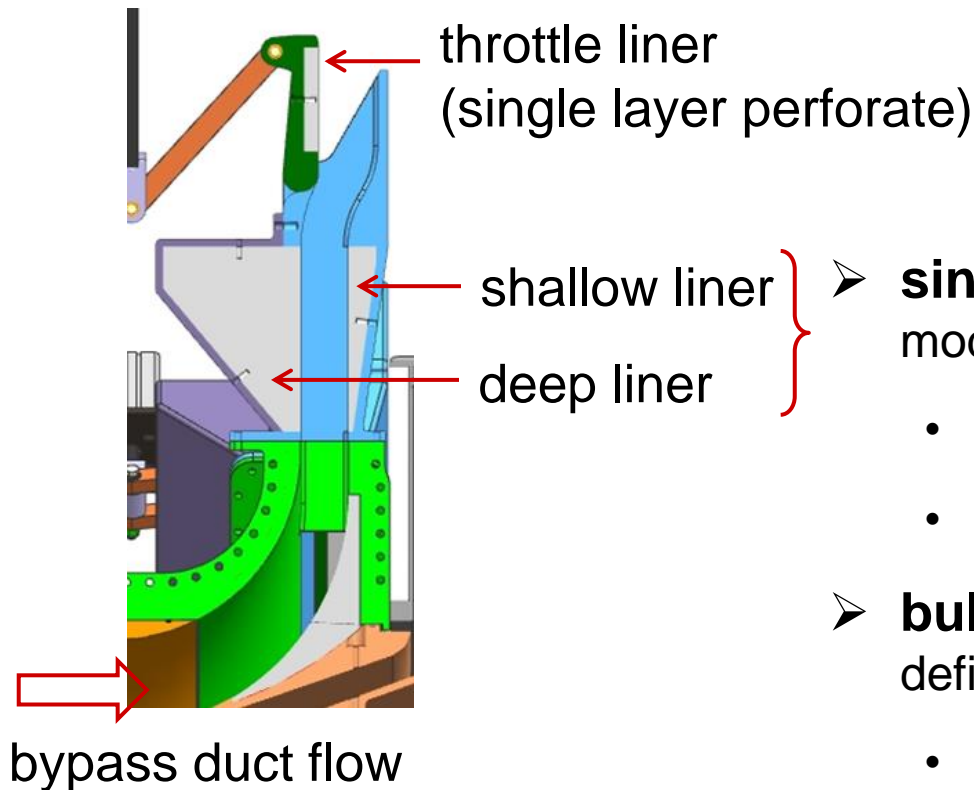


Throttle design: valve noise reduction at source



- **Achieving throttle noise reduction with acoustic liners alone is difficult at lower frequencies**
- **The reduction at source can be achieved with a new flap throttle**

Acoustic liner optimisation: valve and reflected noise reduction



➤ **single/double layer perforate**
modelled using local impedance

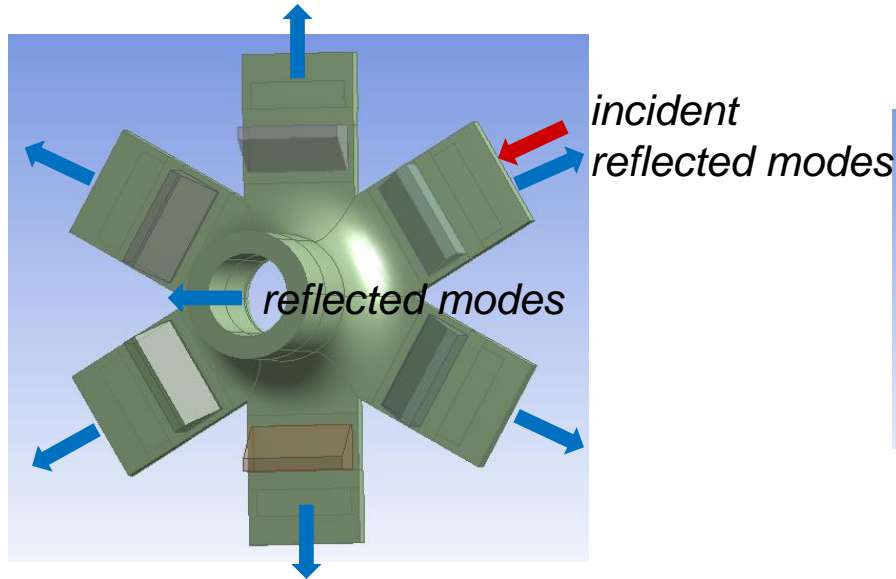
- PROS: difficult to contaminate
- CONS: expensive to replace

➤ **bulk absorbing material**
defined by flow resistivity and facing sheet resistance

- PROS: cheap to replace
- CONS: easy to contaminate

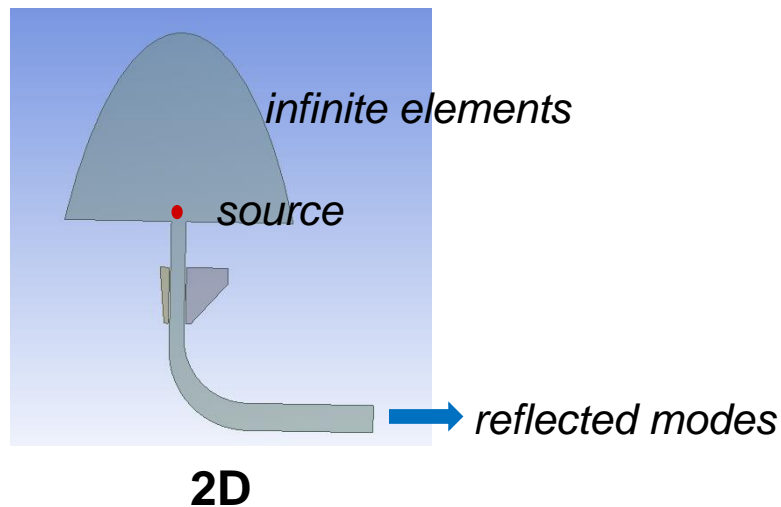
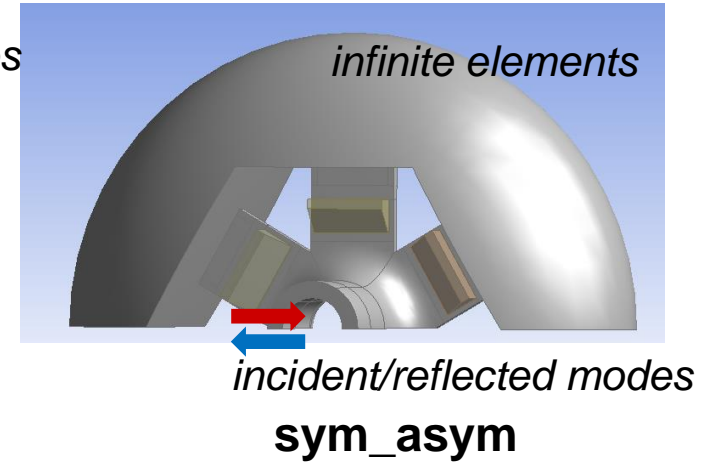
Actran TM models

Throttle noise

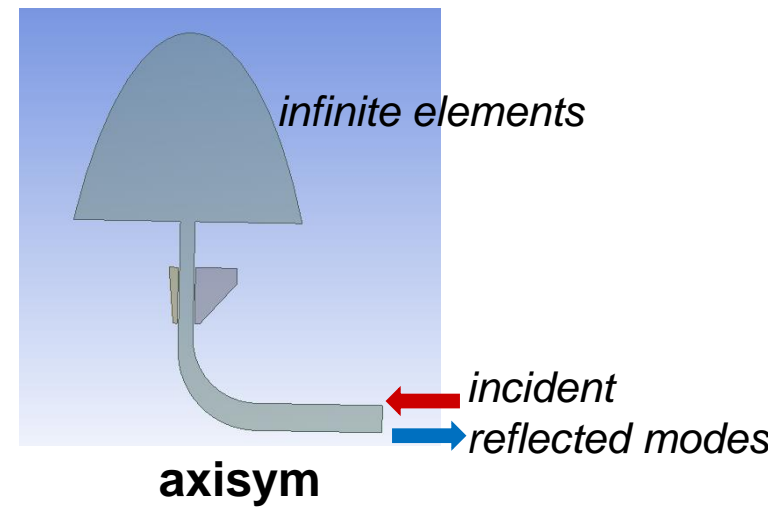


Low frequency
(125 – 1000 Hz)

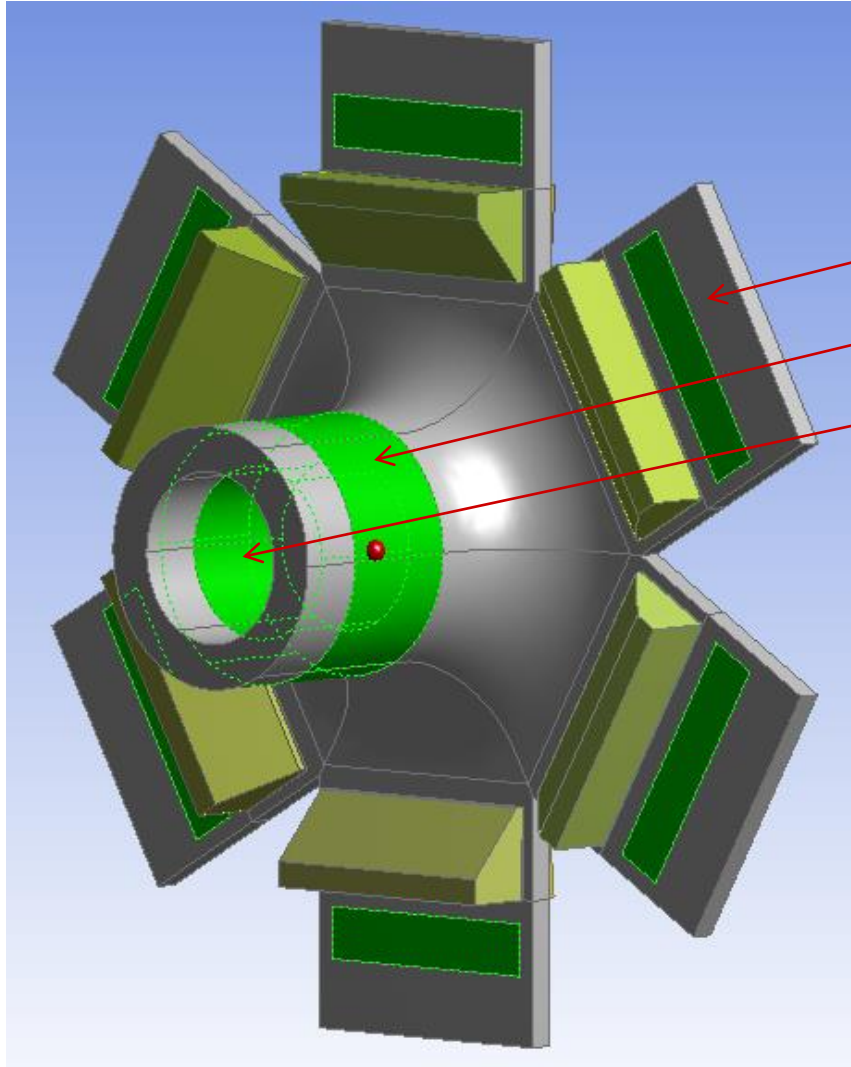
Reflected noise



Optimisation &
High frequency
(1000 – 4000 Hz)



Porous and impedance surfaces



Liners as impedance boundary condition are highlighted in green

1. throttle liner
2. outer bypass duct liner
3. inner bypass duct liner

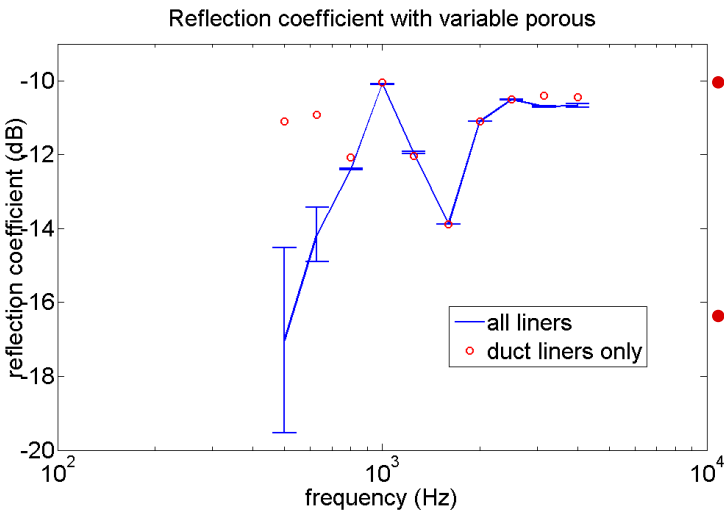
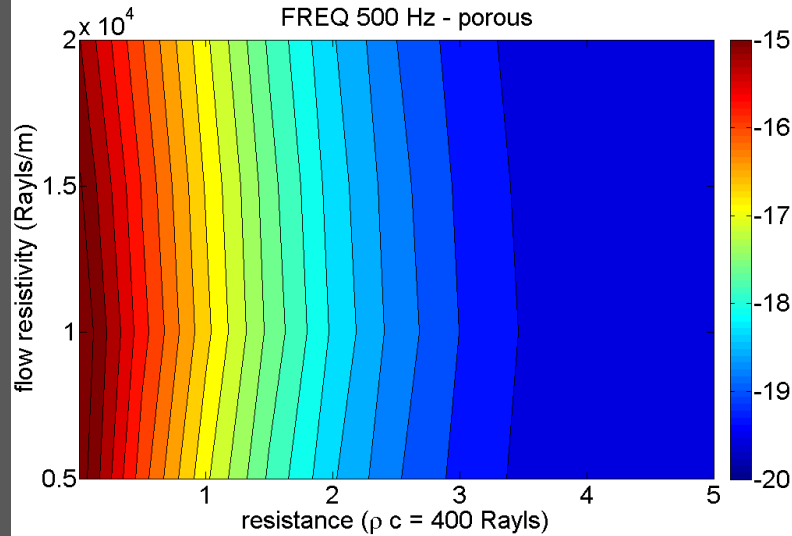
Liner Optimisation

Broadband analysis

High mass flow condition

Reflection coefficient: reflected fan noise

Reflection coefficient @ inlet = $10 * \text{Log} (\text{reflected} / \text{incident modal power})$

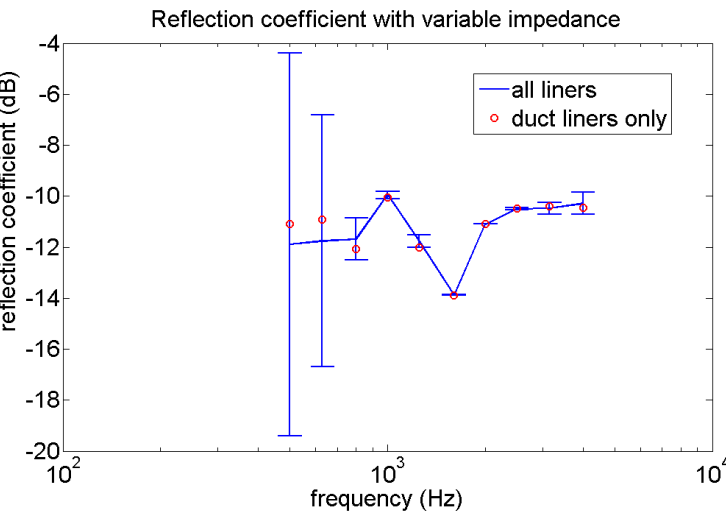
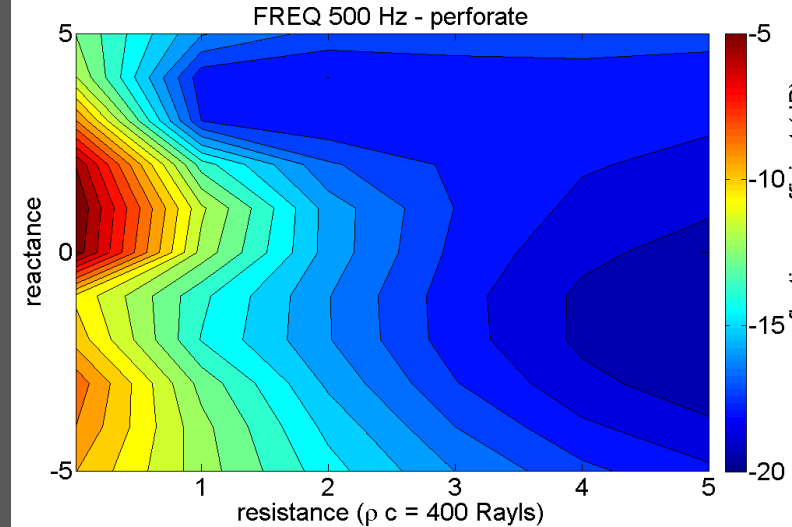


Low frequency

- optimum @ high resistance

High frequency

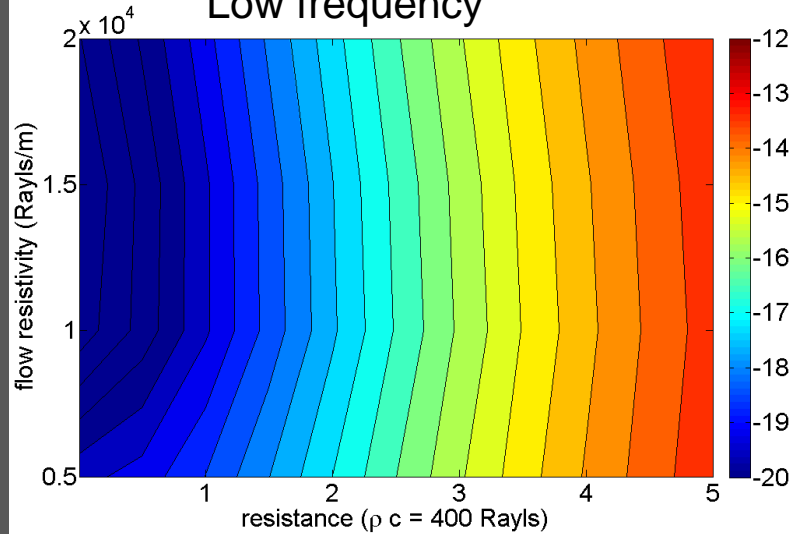
- totally dominated by bypass duct liners



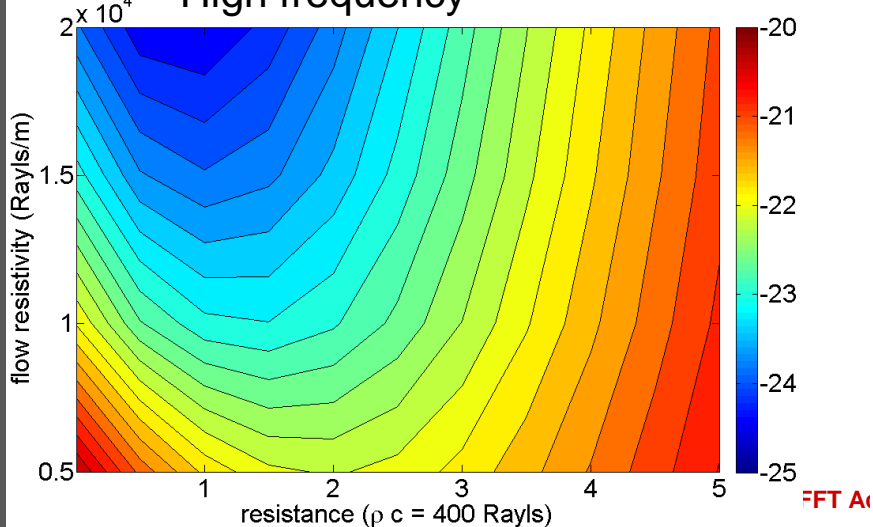
Transmission coefficient: valve noise

Transmission coefficient @ inlet = $10 * \text{Log} (\text{transmitted} / \text{incident power})$

Low frequency



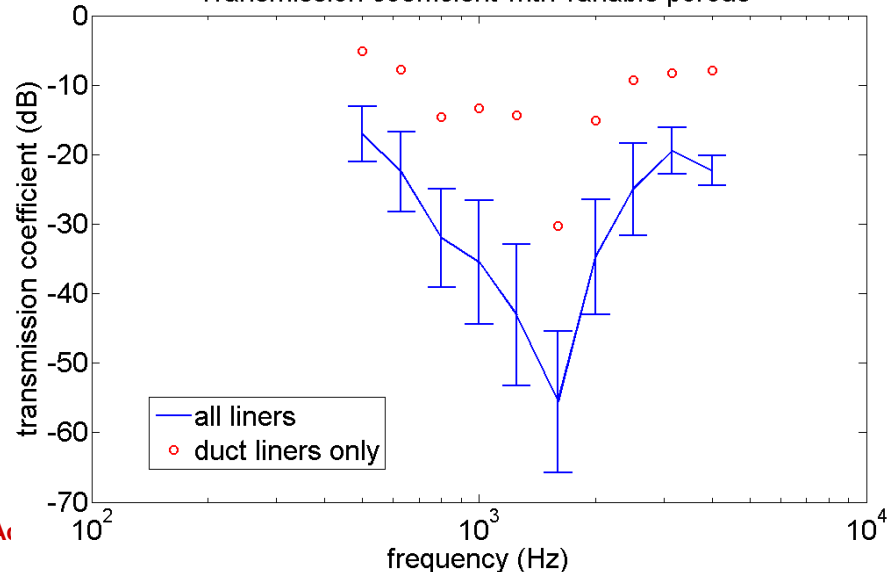
High frequency



Porous liner

- Optimum at low resistance
- High frequency
 - optimum at high flow resistivity

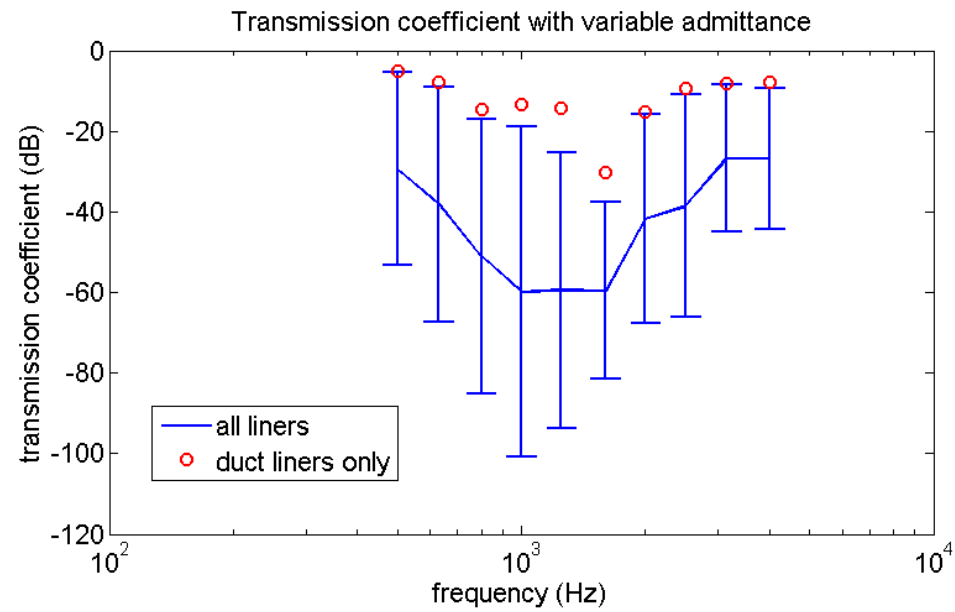
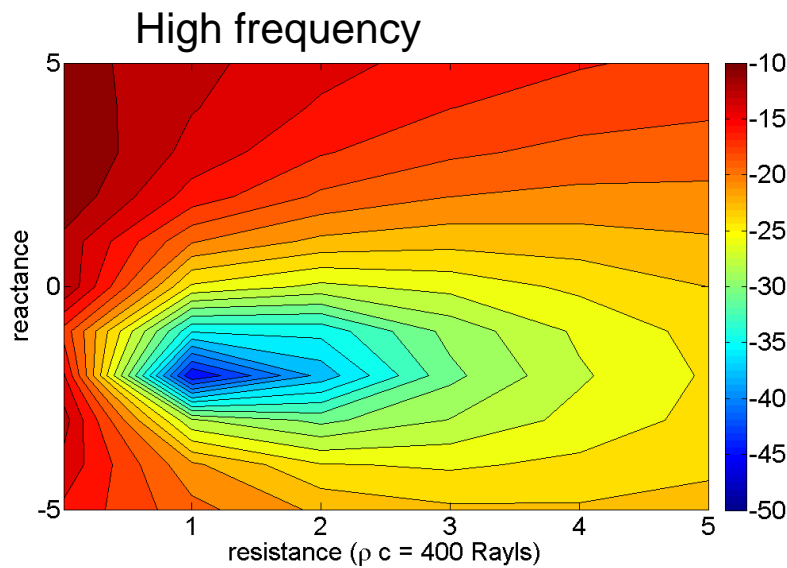
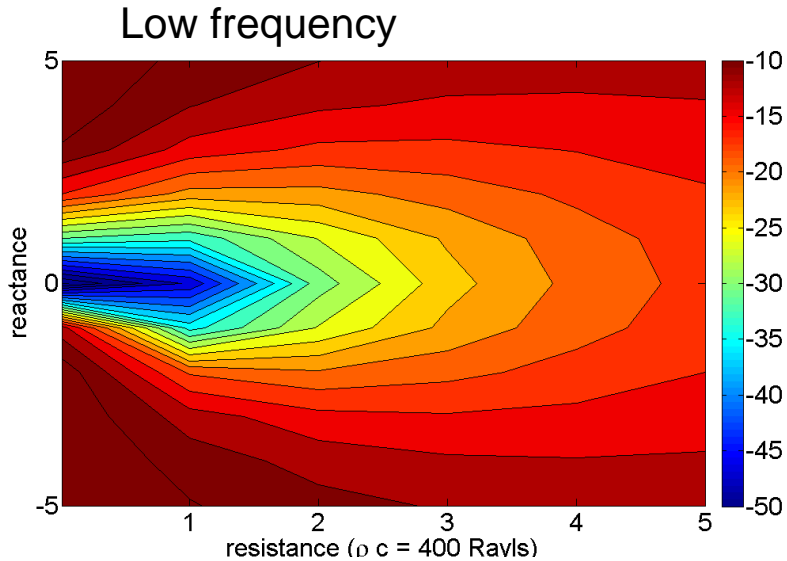
Transmission coefficient with variable porous



Transmission coefficient: valve noise

Perforate liner

- **Low frequency**
 - optimum at very low resistance R and reactance X
- **High frequency**
 - optimum shifting at $R = 1\rho c$, $X = -2\rho c$

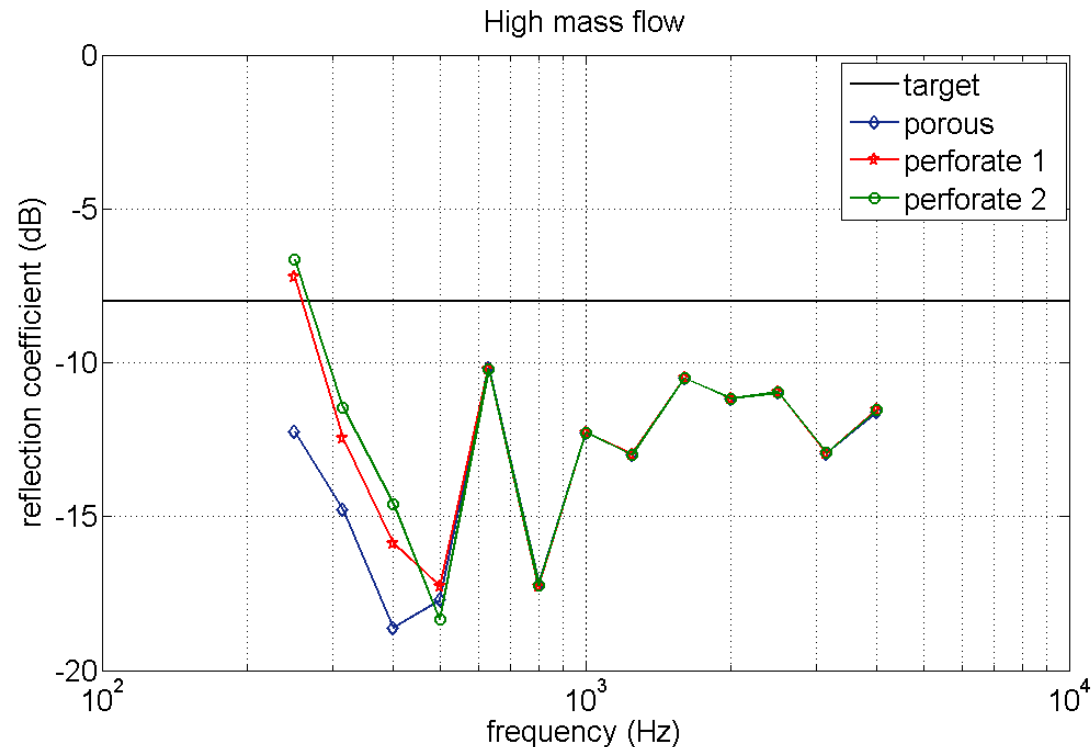


Optimised liner candidates

Liner type	Specification
porous	high flow resistivity low resistance facing sheet
deep perforate	low resistance facing sheet 2 cavity depth candidates
shallow perforate	high resistance facing sheet 2 cavity depth candidates

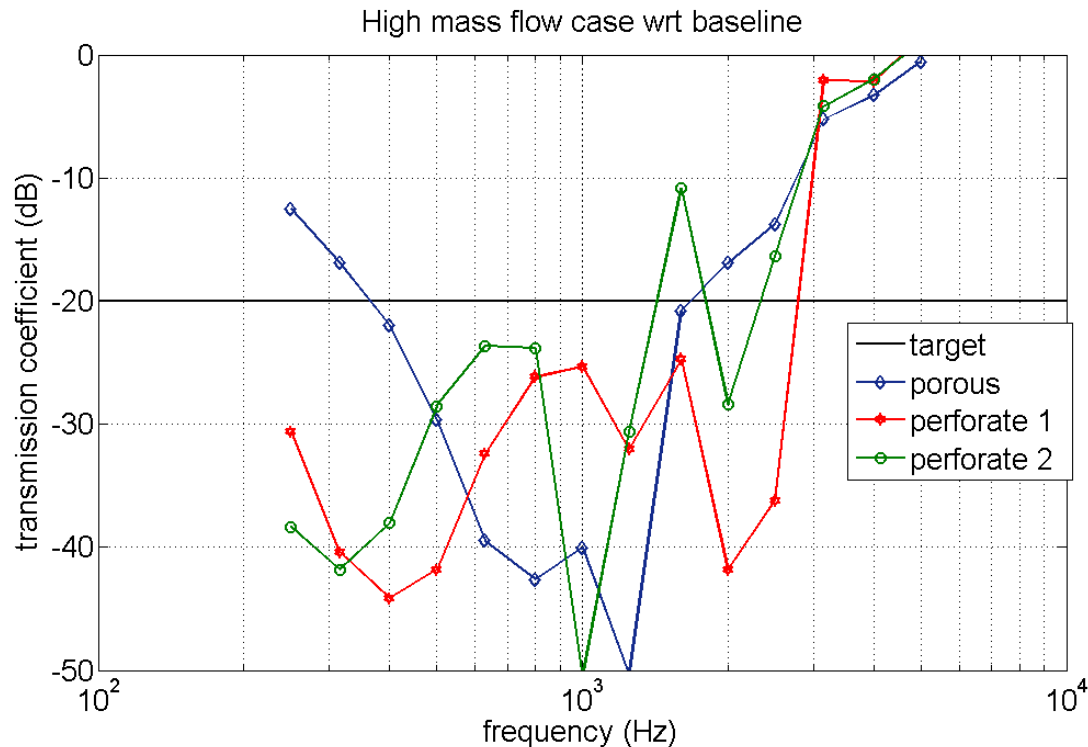
Reflection coefficient: reflected fan noise

- Porous performs better
- No remarkable difference between the two perforate candidates
- Target met by all configurations in (almost) all the frequency range



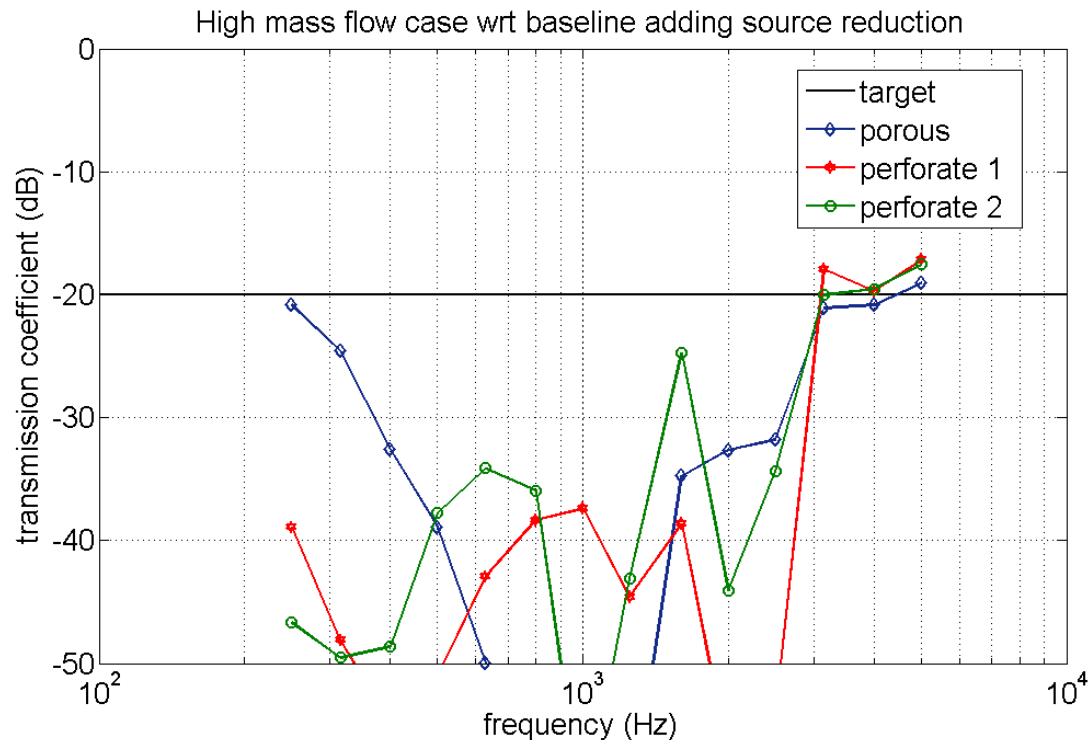
Transmission coefficient: valve noise

- Perforate performs better at low frequency, perforate1 generally better
- Porous performs better at medium frequency
- Target not met at high frequency



Transmission coefficient adding noise reduction at source

- Noise reduction at source due to new throttle design allows to meet the target in the whole frequency range



Computational statistics

- Optimisation via *python* scripting of the session file and *Matlab* post-processing, using the *plt_get* utility
- Computations on 1 processor (Intel Core i7-2600 CPU @ 3.4 GHz, 16GB RAM)

	FE/IE ndof	# porous	# imped	# freq	time per freq slot	total time
2D	100 k	24	66	10	1 min	90 min
Axisym	70 k	24	66	10	15 min	22 h
Half 3D	1,000 k	1	2	7	6 h	18 h
Full 3D	580 k	1	2	7	22 min	1 h

Conclusions

- **Actran TM has been successfully used to support the re-design of the AneCom fan test rig**
- **Liner optimisation via Actran TM allowed to identify 3 liner configurations, whose performance was further analysed to support the final design stage**
- **Reflection and transmission coefficient target was generally met, if noise reduction at source via new throttle was taken into account**
- **Good example of interaction between simulation and experiment insight**